

2/PRTS

METHOD FOR TRIGGERING A RESTRAINT SYSTEM

Background Information

The present invention is based on a method for triggering a restraint system as defined by the preamble to the independent claim.

5 Summary of the Invention

The method of the present invention for triggering a restraint system has the advantage that the threshold value is adapted to the current situation, which is manifested by signal characteristics, by using a combined
10 variable. This variable is determined from a plurality of characteristics of the acceleration signal and/or of the speed signal and/or of a further sensor signal. Thus the threshold value may be adapted to individual signal properties, and as a result of the combination of the
15 various functions which examine these signal properties, only a single variable is employed and is used for adapting the threshold value. The result is a structured intervention into the method of the invention and thus into the tripping algorithm of the invention. This
20 facilitates the intervention into the algorithm and makes for greater clarity. The various individual functions that examine the signal properties are combined using a predetermined logic and then intervene in the algorithm at only one point. Because of the influence at a single
25 point, the requirement for variation for each signal at every instant can also be formulated, and thus a principle for attaining the invention as well as new functionalities can be worked out more systematically. As a result, less time is expended for automatic parameter optimization.

The provisions and refinements recited in the dependent claims permit advantageous improvements to the method recited in the independent claim for triggering a restraint system.

5 It is especially advantageous that the characteristics are determined as a function of various functions for misuse detection, barrier detection, and crash type detection. The chronological conditions pertaining to the crash window, that is, the time when the tripping algorithm
10 begins calculating, are also used for forming characteristics. It is furthermore advantageous that all the characteristics are combined in an adder, at the output of which an amplifier for assessing the variable is advantageously located. This amplifier may be adjusted as
15 a function of certain signal properties. The acceleration signal which is used for the threshold value calculation may advantageously be filtered beforehand using one or more filters, preferably a low-pass filter.

Another advantageous aspect of the invention is that some
20 freely selectable characteristics derived from the acceleration signals, as well as optionally still other sensor signals such as from a passenger sensor system and/or a belt lock, are linked logically together in a matrix, so on the basis of the linkage a decision may be
25 made whether these signals are relevant for the adaptation of the threshold value. Status variables and dynamic variables, in particular, may be linked together. Consequently, dynamic crash characteristics may be assessed, taking the status information into account that
30 is input at the onset of a crash. This assessment may vary between unimportant and important, depending on the sensor signal in question, the vehicle, or the particular restraint device. "Important" or unimportant" here means a corresponding amplification factor; the more important the
35 dynamic crash characteristic is, the higher the amplification factor and thus the greater the influence on

the adaptation of the threshold value. The individual amplification factors are then combined via the entire matrix to form a total amplification factor for adapting the threshold value. The matrix concept makes it simple to add or delete new linkages. This considerably enhances the overall clarity.

It is especially advantageous to use a control unit for performing the method of the present invention for triggering a restraint system.

Brief Description of the Drawings

Exemplary embodiments of the invention are shown in the drawings and explained in further detail in the ensuing description.

Figure 1 shows a block diagram of the method of the present invention; and

Figure 2 shows an example of a signal pattern.

Description of the Preferred Embodiments

In tripping algorithms, the acceleration signal and the integrated acceleration signal are typically processed independently of one another. Under some circumstances, the signal patterns of the acceleration signal and of the speed signal have characteristics that lead to an intervention into the tripping algorithm, in order to take the effect of these characteristics into account. For example, in the event of a hammer blow, which has an acceleration signal of brief duration but high amplitude, the threshold value must be increased sharply, to avert tripping in response to such a hammer blow. An add-on amount in the tripping algorithm is then necessary for that purpose. A plurality of such characteristics in the signals may be detected by signal analysis, and according

to the invention are now added in an adder to make a variable which may be additionally assessed with an amplification factor. The method of the invention permits a structural change in the algorithm of a kind that leads to a considerable simplification of intervention into the algorithm and in particular improves clarity.

Because of the stringent demands for very early signal discrimination using the algorithm, a basic concept which provides for the use of the acceleration signal on the one hand for calculating the threshold value for the speed signal and on the other is determined from the acceleration signal by integration, must be reinforced with further functions. Particularly with the increased use of customer-specific functions, only local solutions to these problems are typically achieved. According to the invention, these solutions are now combined systematically and in structured form. In particular, the overall intervention is scaled in the process. This averts multiplication of the basic algorithm concept, since it is unnecessary to have more than one independent tripping threshold.

In addition, by the described linkage of such status variables as the driver's seat position, the passengers' belt status, or the intrinsic vehicle speed at the onset of the crash with such dynamic variables as defined frequency components of the evaluation of the acceleration signal in the transverse vehicle direction, of the calculated crash severity from the acceleration signal of satellite sensors, or of vehicle-specific functions for detecting certain characteristics in crashes or misuse maneuvers, improved assessment of the dynamic variables during the course of a crash and hence better-adapted protection of the vehicle's passengers are achieved. That is, there is a fusion of sensor values in a matrix.

The following matrix illustrates a first example:

	M 1	Belted	Unbelted
Y Severity	1	Minimal effect on belt tightener threshold	No effect
	2	Maximal effect on belt tightener threshold	No effect
	3	No effect	No effect

The matrix describes the fact that in the course of the
 crash, increased acceleration values in the transverse
 vehicle direction (Y direction) are detected, which
 support the conclusion of an angled or offset crash. This
 Y severity, in Classes 1-3 (column M1), is combined, at
 the moment of detection, with the information about the
 belt status, that is, belted or unbelted. In the unbelted
 situation, the Y severity would be irrelevant for
 calculating the belt tightener threshold, while in the
 belted situation, the Y severity would predict a lateral
 motion of the passenger, and this motion could, for
 instance, influence a two-stage belt tightener system. In
 that case, the combined information is accordingly
 assessed as important, that is, of maximal effect.
 "Irrelevant" means there is no effect. A certain effect is
 indicated by the word "minimal". This is then recalculated
 into a corresponding adaptation of the threshold value for
 the belt tightener.

The following matrix illustrates a second example:

M2	M 3	Driver		Front-seat passenger	
		Seat Close	Seat Far	Seat Close	Seat Far
Low	1	Maximal	None	Maximal	None
	2	Minimal	None	None	None
High	1	Maximal	Maximal	Maximal	Maximal
	2	Maximal	None	None	None

5 In first column M2, high and low speeds are entered in the
second and fourth lines. In second column M3, two
frequency classes are then associated with these two speed
stages. This first frequency class stands for a soft
barrier, and the second frequency class stands for a hard
10 barrier. In the third column, the effect that occurs for a
close far-forward driver's seat position is shown for that
frequency class. In the fourth column, the effect when a
driver's seat is positioned far back is shown. In the
fifth and sixth columns, this is repeated for the front-
15 seat passenger.

In the course of a crash, certain frequency components in
the acceleration signal are detected that indicate a soft
barrier. For them, the frequency components are put into
classifications 1 and 2. At the moment the frequency
20 components are detected, the frequency class is combined
with the seat position information (relatively far forward
or back) and the intrinsic speed at the onset of the
crash. Since separate tripping thresholds for the driver
and the front-seat passenger are calculated in the
25 tripping algorithm, it is possible, depending on the
calculated frequency class of the crash, to exert a
varying influence on the tripping for a driver seated very
far forward and a front-seat passenger seated very far

back; the combination with the forward-seated passenger could be assessed as very important, and the combination with the rearward-seated passenger could be assessed as less important.

5 If a relatively low speed in combination with a driver seated very far forward is now detected, then the two-stage front air bag tripping could be desensitized because of the excessive risk of injury, while at a high speed, the front airbag must be tripped earlier for a passenger
10 seated farther forward than for a passenger seated farther back.

Figure 1, in a block diagram, shows the method of the present invention for triggering a restraint system. An acceleration signal a_x is input at point 1 in the block
15 diagram. This acceleration signal is generated here in the control unit by an acceleration sensor or a combination of acceleration sensors disposed at angles to one another. Alternatively or in addition, it is possible for the acceleration signal to be generated by a remote sensor or
20 so-called satellite sensor. A satellite sensor of this kind may be disposed in the side and/or at the front of the vehicle.

Typically, micromechanical acceleration sensors that function piezoelectrically are used as sensors. However,
25 mechanical sensors or other sensors that are suitable for picking up the acceleration are also possible. The acceleration signal is then used in two independent paths, on the one hand by an integration 2 for calculating a speed ΔV_x and on the other for calculating a threshold
30 value 4.

Before threshold-value calculation 4, filtering 3 of acceleration signal a_x is performed. Typically, a low-pass filter is used as the filter. Signal $a_{x\text{filter}}$ is then present and enters into the calculation of the acceleration

signal. An integration time 5 is used as a further input parameter into threshold-value calculation 4.

Threshold value ΔV_{XTH} thus determined is adapted by a subtractor 6 using correction value ΔV_{ADD-ON} . Correction value ΔV_{ADD-ON} has been generated by an amplifier 7. Amplifier 7 has amplified a signal from an adder 8. That is, it has performed weighting.

A plurality of characteristics or functions 9-14 are connected to the inputs of adder 8. These include the signal from an up-front sensor 9, an add-on amount for a deformable barrier 11, taking integration window 13 during the collision into account, and further taking hammer blow 14 into account. All these signal characteristics, which are derived from acceleration signal a_x or integration signal ΔV_x , are examined by these functions for their significance in view of varying the threshold value. It is possible for the individual functions to be weighted by their own amplification factors, and this weighting may be signal-dependent.

The adapted threshold value downstream of subtractor 6 then leads to a comparison, in a comparator 15, of threshold value $\Delta V_{XTH-ADD}$ with integrated acceleration signal ΔV_x . As a function of this comparison, the restraint device is then triggered via an output 16. In other words, if signal ΔV_x is above the threshold value, then a tripping situation is detected, and optionally as a function of plausibility, the restraint device, that is, a belt tightener or an air bag, should be triggered.

Figure 2, in a time and speed graph, shows the course of the threshold values with and without correction and the course of the integrated acceleration signal. It can be seen that integrated acceleration signal ΔV_x up to time 17 is higher than both adapted threshold value $\Delta V_{XADD-ON}$ and threshold value ΔV_{XTH} that is output by threshold-value

calculation 4. From this time 17 onward, however, the integrated acceleration signal is below the corrected threshold value, so that comparator 15 does not output any triggering signal for the restraint system. Without the
5 correction by subtractor 6, integrated acceleration signal ΔV_x would be above threshold value ΔV_{XTH} until time 16. It has thus been shown that tripping could be avoided by the signal analysis.

10 Alternatively, it is possible to use a system with a criterion that is compared with a fixed threshold. This threshold may then be varied by additional criteria. This makes it possible to replace a combination of individual criteria.